



Aalto University

# Linearisation of nonlinear models: Example

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# Example I

## Linearisation of nonlinear models

## Example I

Consider two chemical species  $A$  and  $B$  in a solvent feed entering a chemical reactor

- The two species react to form a third one, the product component  $P$
- $A + 2B \rightarrow P$

Liquid-phase chemical reactor

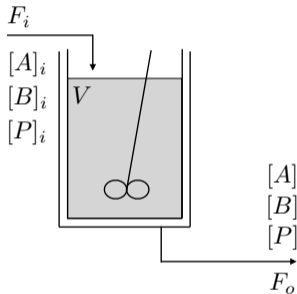
↪ Volume  $V(t)$

Temperature is constant

↪  $T(t) = \text{constant}$

Volumetric flow-rates

↪  $F_i(t)$  and  $F_o(t)$



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Assuming perfect mixing, our main interest is in the concentrations inside the reactor

- ↪ The concentration of species as a function of time  $[A](t)$ ,  $[B](t)$ , and  $[P](t)$
- (Interest also in  $V(t)$ , because we do not want to flood/dry the tank)

## Example I (cont.)

### Total mass balance

$$\begin{aligned}
 \underbrace{\frac{dM(t)}{dt}}_{\text{(mass/time)}} &= \underbrace{\frac{dV(t)\rho_0(t)}{dt}}_{\text{(volume} \times \text{(mass / volume) / time)}} \\
 &= \underbrace{\rho_i(t)}_{\text{(mass / volume)}} \underbrace{F_i(t)}_{\text{(volume / time)}} - \underbrace{\rho_o(t)}_{\text{(mass / volume)}} \underbrace{F_o(t)}_{\text{(volume / time)}}
 \end{aligned}$$

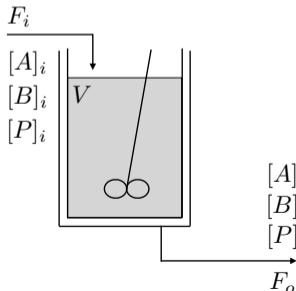
Assuming (!) that the density does not depend on the concentration of  $A$ ,  $B$  and  $P$ , we get

$$\rho_o(t) = \rho_i(t) = \rho \quad \rightsquigarrow \quad \rho \neq \rho(t)$$

$\rightsquigarrow$  Density does not depend on time

The resulting total mass balance,

$$\rightsquigarrow \quad \frac{dV(t)}{dt} = F_i(t) - F_o(t)$$



## Example I (cont.)

### Component mass balance

Let  $[A]$ ,  $[B]$  and  $[P]$  be molar concentrations (moles/volume) of species  $A$ ,  $B$  and  $P$

- Based on some kinetic modelling, we are given the stoichiometric equation



Assuming that there is no product  $P$  in the feed ( $[P]_i(t) = 0$  for all  $t \geq t(0)$ ), we have

$$\frac{dV(t)[A](t)}{dt} = F_i(t)[A]_i(t) - F_o(t)[A]_o(t) + V(t)r_A(t)$$

$$\frac{dV(t)[B](t)}{dt} = F_i(t)[B]_i(t) - F_o(t)[B]_o(t) + V(t)r_B(t)$$

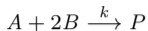
$$\frac{dV(t)[P](t)}{dt} = F_i(t)\cancel{[P]_i(t)} - F_o(t)[P]_o(t) + V(t)r_P(t)$$

$r_A(t)$ ,  $r_B(t)$  and  $r_P(t)$  denote generation/consumption rates of species  $A$ ,  $B$  and  $P$

- Given per unit volume, and assume we know the reaction rate constant  $k$

$$\rightsquigarrow \left( \frac{\text{moles}}{\text{time}} \right) / \text{volume}$$

## Example I (cont.)



We can assume that the reaction rate per unit volume for component  $A$  is second order

- We can also assume that it depends on the composition of both  $A(t)$  and  $B(t)$

$$r_A(t) = -k[A](t)[B](t), \quad (\text{rate of generation of } A, \text{ per unit volume})$$

The stoichiometric equation tells us that one mole of  $A$  reacts with two moles of  $B$

- ... to produce one mole of  $P$

We can also write the generation rates (per unit volume) for the remaining species

$$r_B(t) = -2k[A](t)[B](t)$$

$$r_P(t) = k[A](t)[B](t)$$

At this point, we need to substitute their expressions in the mass balances

## Example I (cont.)

Consider the mass balance for component  $A$  and differentiate with respect to time

$$\begin{aligned}\frac{dV(t)[A](t)}{dt} &= V(t)\frac{d[A](t)}{dt} + [A](t)\frac{dV(t)}{dt} \\ &= F_i(t)[A]_i(t) - F_o(t)[A](t) - \underbrace{V(t)k[A](t)[B](t)}_{-r_A}\end{aligned}$$

Dividing by  $V(t)$  and rearranging terms, we get

$$\frac{d[A](t)}{dt} = \frac{F_i(t)}{V(t)}[A]_i(t) - \frac{F_o(t)}{V(t)}[A](t) - \frac{V(t)}{V(t)}k[A](t)[B](t) - \frac{1}{V(t)}\frac{dV(t)}{dt}[A](t)$$

From the total mass balance, we know that  $\frac{dV(t)}{dt} = F_i(t) - F_o(t)$

$$\begin{aligned}\frac{d[A](t)}{dt} &= \frac{F_i(t)}{V(t)}[A]_i(t) - \cancel{\frac{F_o(t)}{V(t)}[A](t)} - k[A](t)[B](t) - \frac{F_i(t)}{V(t)}[A](t) + \cancel{\frac{F_o(t)}{V(t)}[A](t)} \\ &= \frac{F_i(t)}{V(t)}\left([A]_i(t) - [A](t)\right) - k[A](t)[B](t)\end{aligned}$$

## Example I (cont.)

We can proceed similarly for component  $B$  and component  $P$  to get their dynamics

$$\rightsquigarrow \frac{d[B](t)}{dt} = \frac{F_i(t)}{V(t)} \left( [B]_i(t) - [B](t) \right) - 2k[A](t)[B](t)$$
$$\rightsquigarrow \frac{d[P](t)}{dt} = \frac{F_i(t)}{V(t)} \left( \underbrace{[P]_i(t)}_{=0} - [P](t) \right) + k[A](t)[B](t)$$



## Example I (cont.)

Altogether, we have model equations involving 4 state variables and 4 input variables

$$\begin{aligned}\frac{d[A](t)}{dt} &= \frac{F_i(t)}{V(t)} ([A]_i(t) - [A](t)) - k[A](t)[B](t) \\ \frac{d[B](t)}{dt} &= \frac{F_i(t)}{V(t)} ([B]_i(t) - [B](t)) - 2k[A](t)[B](t) \\ \frac{d[P](t)}{dt} &= -\frac{F_i(t)}{V(t)} [P](t) + k[A](t)[B](t) \\ \frac{dV(t)}{dt} &= F_i(t) - F_o(t)\end{aligned}$$

The state equations of the model consists of four first-order differential equations

- ↪ Thus four state variables, they are associated with the derivatives
- ↪ Variables  $V(t)$ ,  $[A](t)$ ,  $[B](t)$  and  $[P](t)$  have dynamics

As for the four (five) input variables, some are controls others are disturbances

- ↪  $F_i(t)$ ,  $F_o(t)$ ,  $[A]_i(t)$ ,  $[B]_i(t)$  (and  $[P]_i(t)$ )

## Example I (cont.)

Four initial conditions (at  $t = 0$ ) are needed for determining the temporal evolution

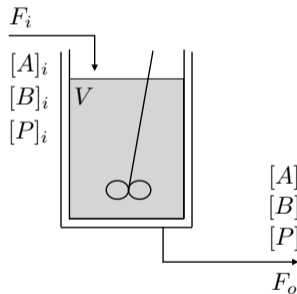
↪  $V(0)$ ,  $[A](0)$ ,  $[B](0)$  and  $[P](0)$

To determine the temporal evolution, we also need to set the inputs to be applied

↪  $F_i(t)$ ,  $F_o(t)$ ,  $[A]_i(t)$ ,  $[B]_i(t)$  (and  $[P]_i(t)$ )

- From the initial time  $t = 0$  onwards

$$\begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} = \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V} ([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V} ([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V} [P] + k[A][B] \end{bmatrix}$$



Note how the state equations of the state-space model contains also a parameter,  $k$

↪ We assumed it to be time-invariant (that is,  $k \neq k(t)$ )

## Example I (cont.)

$$\begin{aligned} \begin{bmatrix} \dot{V} \\ [\dot{A}] \\ [\dot{B}] \\ [\dot{P}] \end{bmatrix} &= \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V} ([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V} ([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V} [P] + k[A][B] \end{bmatrix} \\ &= \begin{bmatrix} f_1(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_2(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_3(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_4(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \end{bmatrix} \end{aligned}$$

↪ For the state variables,  $x(t)$

$$x(t) = \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ x_4(t) \end{bmatrix} = \begin{bmatrix} V(t) \\ [A](t) \\ [B](t) \\ [P](t) \end{bmatrix}$$

## Example I (cont.)

$$\begin{aligned} \begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} &= \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V}([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V}([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V}[P] + k[A][B] \end{bmatrix} \\ &= \begin{bmatrix} f_1(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_2(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_3(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_4(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \end{bmatrix} \end{aligned}$$

↪ For the input variables,  $u(t)$

$$u(t) = \begin{bmatrix} u_1(t) \\ u_2(t) \\ u_3(t) \\ u_4(t) \end{bmatrix} = \begin{bmatrix} F_i(t) \\ F_o(t) \\ [A]_i(t) \\ [B]_i(t) \end{bmatrix},$$

## Example I (cont.)

$$\begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} = \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V} ([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V} ([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V} [P] + k[A][B] \end{bmatrix}$$

$$= \begin{bmatrix} f_1(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_2(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_3(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_4(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \end{bmatrix}$$

↪ For the parameter(s),  $\theta_x$

$$\theta_x = \begin{bmatrix} \theta_1^x \\ \theta_2^x \end{bmatrix} = \begin{bmatrix} k \\ B \end{bmatrix}$$

Strictly speaking,  $B$  is embedded in the state variable  $V$  and hence not a parameter

- We still need to know it's value to be able to do computations

## Example I (cont.)

$$\begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} = \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V}([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V}([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V}[P] + k[A][B] \end{bmatrix}$$

For compactness, we can now write the state-space equations using the control notation

$$\underbrace{\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix}}_{\dot{x}} = \underbrace{\begin{bmatrix} f_1(x, u | \theta_x) \\ f_2(x, u | \theta_x) \\ f_3(x, u | \theta_x) \\ f_4(x, u | \theta_x) \end{bmatrix}}_{f(x, u | \theta_x)} = \begin{bmatrix} u_1 - u_2 \\ \frac{u_1}{x_1}(u_3 - x_2) - kx_2x_3 \\ \frac{u_1}{x_1}(u_4 - x_3) - 2kx_2x_3 \\ -\frac{u_1x_4}{x_1} + kx_2x_3 \end{bmatrix}$$

## Example I (cont.)

Let  $x'(t) = [x(t) - x_{SS}(t)]$ ,  $u'(t) = [u(t) - u_{SS}(t)]$ , for some steady-state  $(x_{SS}, u_{SS})$

We write a linearised model,  $\dot{x}'(t) = Ax'(t) + Bu'(t)$  by computing matrix  $A$  and  $B$

$$A = \begin{bmatrix} \left. \frac{\partial f_1(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_2(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_3(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_4(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \end{bmatrix}$$

$$B = \begin{bmatrix} \left. \frac{\partial f_1(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_2(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_3(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_4(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \end{bmatrix}$$

## Example I (cont.)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} u_1 - u_2 \\ \frac{u_1}{x_1}(u_3 - x_2) - kx_2x_3 \\ \frac{u_1}{x_1}(u_4 - x_3) - 2kx_2x_3 \\ -\frac{u_1x_4}{x_1} + kx_2x_3 \end{bmatrix}$$

By taking the partial derivatives of  $f$  with respect to the state variables  $x$ , we obtain

$$A = \begin{bmatrix} 0 & 0 & 0 & 0 \\ -\frac{u_1(u_3 - x_2)}{x_1^2} \Big|_{x_{SS}, u_{SS}} & \left(-\frac{u_1}{x_1} - kx_3\right) \Big|_{x_{SS}, u_{SS}} & -kx_2 \Big|_{x_{SS}, u_{SS}} & 0 \\ -\frac{u_1(u_4 - x_3)}{x_1^2} \Big|_{x_{SS}, u_{SS}} & -2kx_3 \Big|_{x_{SS}, u_{SS}} & \left(-\frac{u_1}{x_1} - 2kx_2\right) \Big|_{x_{SS}, u_{SS}} & 0 \\ \frac{u_1x_4}{x_1^2} \Big|_{x_{SS}, u_{SS}} & k & kx_2 \Big|_{x_{SS}, u_{SS}} & -\frac{u_1}{x_1} \Big|_{x_{SS}, u_{SS}} \end{bmatrix}$$

For some fixed point  $(x_{SS}, u_{SS})$



## Example I (cont.)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} u_1 - u_2 \\ \frac{u_1}{x_1}(u_3 - x_2) - kx_2x_3 \\ \frac{u_1}{x_1}(u_4 - x_3) - 2kx_2x_3 \\ -\frac{u_1x_4}{x_1} + kx_2x_3 \end{bmatrix}$$

By taking the partial derivatives of  $f$  with respect to the input variables  $u$ , we obtain

$$B = \begin{bmatrix} 1 & -1 & 0 & 0 \\ \left. \frac{u_3 - x_2}{x_1} \right|_{x_{SS}, u_{SS}} & 0 & \left. \frac{u_1}{x_1} \right|_{x_{SS}, u_{SS}} & 0 \\ \left. \frac{u_4 - x_3}{x_1} \right|_{x_{SS}, u_{SS}} & 0 & 0 & \left. \frac{u_1}{x_1} \right|_{x_{SS}, u_{SS}} \\ \left. -\frac{x_4}{x_1} \right|_{x_{SS}, u_{SS}} & 0 & 0 & 0 \end{bmatrix}$$

Again, for some fixed point  $(x_{SS}, u_{SS})$

The nonlinear model linearised around  $(x_{SS}, u_{SS})$

$$\dot{x}'(t) = \begin{bmatrix} 0 & 0 & 0 & 0 \\ -\frac{u_1(u_3 - x_2)}{x_1^2} & -\frac{u_1}{x_1} - kx_3 & -kx_2 & 0 \\ -\frac{u_1(u_4 - x_3)}{x_1^2} & -2kx_3 & -\frac{u_1}{x_1} - 2kx_2 & 0 \\ \frac{u_1 x_4}{x_1^2} & k & kx_2 & -\frac{u_1}{x_1} \end{bmatrix}_{SS} x'(t) + \begin{bmatrix} 1 & -1 & 0 & 0 \\ \frac{u_3 - x_2}{x_1} & 0 & \frac{u_1}{x_1} & 0 \\ \frac{u_4 - x_3}{x_1} & 0 & 0 & \frac{u_1}{x_1} \\ \frac{x_4}{x_1} & 0 & 0 & 0 \end{bmatrix}_{SS} u'(t)$$

Assuming that we can measure all the state variables, for  $y'(t) = y(t) - y_{SS}$  we have

$$y'(t) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} x'(t) + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} u'(t)$$

What is  $y_{SS}$ ?

